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Plasma-sprayed CaTiSiO_5 ceramic coating on Ti-6Al-4V with excellent bonding strength, stability and cellular bioactivity

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Novel Ca-Si-Ti-based sphene (CaTiSiO_5) ceramics possess excellent chemical stability and cytocompatibility. The aim of this study was to prepare sphene coating on titanium alloy (Ti-6Al-4V) for orthopaedic applications using the plasma spray method. The phase composition, surface and interface microstructure, coating thickness, surface roughness and bonding strength of the plasma-sprayed sphene coating were analysed using X-ray diffraction, scanning electron microscopy, atomic force microscopy and the standard mechanical testing of the American Society for Testing and Materials, respectively. The results indicated that sphene coating was obtained with a uniform and dense microstructure at the interface of the Ti-6Al-4V surface and the thickness and surface roughness of the coating were approximately 150 and 10 μm , respectively. Plasma-sprayed sphene coating on Ti-6Al-4V possessed a significantly improved bonding strength and chemical stability compared with plasma-sprayed hydroxyapatite (HAp) coating. Plasma-sprayed sphene coating supported human osteoblast-like cell (HOB) attachment and significantly enhanced HOB proliferation and differentiation compared with plasma-sprayed HAp coating and uncoated Ti-6Al-4V. Taken together, plasma-sprayed sphene coating on Ti-6Al-4V possessed excellent bonding strength, chemical stability and cellular bioactivity, indicating its potential application for orthopaedic implants.

Keywords: plasma spraying; surface modification; sphene; osteoblasts; titanium alloy

1. INTRODUCTION

The prevalence of primary and revision of total hip and knee arthroplasties increased steadily between 1990 and 2002 (Kurtz *et al.* 2005), and is expected to increase over the next two decades (Kurtz *et al.* 2007). Recently, the rate of joint replacement surgery has increased by 5–10 per cent per year, and over the past 20 years it has increased more than 10 per cent per year. Moreover, as many as 25 per cent of cementless hip replacements survive less than 10 years in young patients (Peter *et al.* 2005). Revision operations are mainly due to aseptic loosening of the implant following erosion of the supporting bone. Consequently, there is a need to develop new biocompatible surfaces that will anchor the implant device to the bone tissue in a strong and enduring manner.

A well-established primary biomaterial for orthopaedic implants is Ti-6Al-4V, a titanium alloy; however, it does not functionally integrate into bone. Various surface modification methods have been proposed for

Ti-6Al-4V. The aim has been to enhance osseointegration and thereby interlock the implant with the surrounding skeletal tissue, which will provide a stable interface strong enough to support lifelong functional loading. Previous studies have shown that surface chemical modification of Ti-6Al-4V significantly enhanced the initial response, phenotype and signalling pathways of human osteoblasts (Zreiqat *et al.* 1999, 2002, 2005; Harle *et al.* 2006). Although these approaches have had some success, their major drawbacks are the slow rates of osseointegration and poor mechanical anchorage in challenging clinical cases (Sporer & Paprosky 2005).

Ti-6Al-4V coated with bioactive ceramics such as plasma-sprayed hydroxyapatite (HAp; Ha *et al.* 1998; Harle *et al.* 2006; Balani *et al.* 2007) and calcium silicate (CaSiO_3 ; Liu *et al.* 2001; Xue *et al.* 2005) showed improved stability of Ti-6Al-4V, providing a strong interface between the coating and the alloy and enhanced bone growth and mineralization (Soballe *et al.* 1991). However, these too have drawbacks (Kweh *et al.* 2002; Liu *et al.* 2004a,b; Xue *et al.* 2004). A crucial problem of Ti-6Al-4V-coated HAp is the poor bonding strength with the metal substrate due to the

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mismatch of thermal expansion coefficient between HAp and Ti-6Al-4V (Liu *et al.* 2004*a,b*). The high residual stress resulting from the mismatch of the thermal expansion coefficient between HAp ($13.3 \times 10^{-6} \text{ K}^{-1}$) and Ti-6Al-4V (8.4×10^{-6} to $8.8 \times 10^{-6} \text{ K}^{-1}$) is thought to be responsible for the higher tensile stress and microcracks at the interface, which decreases the bonding strength between the two materials (HAp and Ti-6Al-4V) and limits their long-term survival (Kweh *et al.* 2002; Liu *et al.* 2004*a,b*; Xue *et al.* 2004).

Owing to their good bioactivity, CaSiO₃ ceramics have been used as coating on Ti-6Al-4V for biomedical applications (De Aza *et al.* 2000; Liu *et al.* 2004*a,b*; Xue *et al.* 2005). The results showed enhanced bonding strength of the plasma-sprayed CaSiO₃ coating, compared with HAp (e.g. Kweh *et al.* 2002; Liu *et al.* 2004*a,b*; Xue *et al.* 2005). However, like HAp, CaSiO₃ coatings have drawbacks, including their low chemical stability leading to degradation and instability of the coating after implantation (Liu *et al.* 2004*a,b*). Although CaSiO₃ coatings produced good bioactivity and enhanced short-term osseointegration properties of the implant (Xue *et al.* 2005), their poor chemical stability continues to be a major drawback and their long-term stability is questionable (Liu & Ding 2002; Wu *et al.* 2007*a,b*).

Sphene is a Ca-, Ti- and Si-containing mineral (Wu *et al.* 2007*a,b*) and, recently, we found that coating Ti-6Al-4V with sphene ceramic using the sol-gel method resulted in an improved adhesion strength and chemical stability of the coating compared with the sol-gel HAp coating (Wu *et al.* 2007*a,b*, 2008*a-c*, 2008). High temperature (more than 1000°C) is required to obtain a completely sintered and dense sphene, which is necessary to obtain good bonding strength of the coating. However, it cannot be applied when the sol-gel method is used to coat dense sphene on metals. Moreover, a temperature of more than 900°C will seriously oxidize and damage the Ti-6Al-4V surface. Plasma spraying, another common method often used to coat ceramics, avoids the above-mentioned drawbacks of the sol-gel method problem. Plasma spraying directly imposes extremely high temperatures on ceramic particles to melt/sinter them, but it avoids the direct exposure to high temperature of the Ti alloy substrate and hence avoids damaging the Ti alloy. The high temperature produced by the plasma spraying method is able to sinter and produce sphene coating with denser microstructure, compared with the sol-gel method. This will significantly improve the bonding strength of the coating on the Ti alloy (Liu *et al.* 2004*a,b*). In addition, the thermal expansion coefficient of sphene ($6 \times 10^{-6} \text{ K}^{-1}$) is similar to that of Ti-6Al-4V (8.4×10^{-6} to $8.8 \times 10^{-6} \text{ K}^{-1}$). Therefore, in the present study, we plasma sprayed sphene coating onto Ti-6Al-4V in an attempt to improve the bonding strength and compared their properties with sol-gel sphene coating and currently used plasma-sprayed HAp coating.

It is known that chemical composition (Zreiqat *et al.* 2005; Harle *et al.* 2006; Wei *et al.* 2008) and surface topography (Masaki *et al.* 2005; Liu *et al.* 2008) of the biomaterial can alter the cellular responses substantially. Recently, we showed that excellent human

Table 1. Plasma spraying parameters.

argon plasma gas flow rate (slpm)	40
hydrogen plasma gas flow rate (slpm)	10
spray distance (mm)	100
argon powder carrier gas (slpm)	3.5
current (A)	600
voltage (V)	70

osteoblast-like cell (HOB) activity was obtained when the cells were cultured on dense sphene ceramic discs (Wu *et al.* 2007*a,b*). However, plasma-sprayed sphene coating has significantly different surface topography, roughness and microstructure compared with sphene ceramic discs, which could influence HOB activity. Therefore, in the present study, we aim to determine the effect of plasma-sprayed sphene coating on HOB attachment, proliferation and differentiation and compare their response with those cultured on HAp coating.

2. MATERIALS AND METHODS

2.1. Preparation of plasma-sprayed coating

Sphene powders were synthesized by the sol-gel process using tetraethyl orthosilicate ((C₂H₅O)₄Si, TEOS; Sigma Aldrich, USA), titanium (IV) butoxide (Ti(O(CH₂)₃CH₃)₄, Ti(Bu)₄; Sigma Aldrich, USA) and calcium nitrate tetrahydrate (Ca(NO₃)₂·4H₂O; Sigma Aldrich, USA), as detailed previously (Wu *et al.* 2007*a,b*). Briefly, TEOS and Ti(Bu)₄ were mixed with ethanol and 2 M HNO₃ (molar ratio: TEOS/Ti(Bu)₄/ethanol/HNO₃=1:1:10:0.08) and hydrolysed for 30 min while stirring. Ca(NO₃)₂·4H₂O was added to the mixture (molar ratio: TEOS/Ti(Bu)₄/Ca(NO₃)₂·4H₂O=1:1:1), and the reactants were stirred for 5 hours at room temperature followed by incubation at 60°C for 1 day before drying at 100°C for 2 days. The obtained dry gel was ground and transferred into a corundum crucible and calcined at 1100°C for 3 hours.

The calcined sphene powders were sieved to 80 mesh to get particles of 45–200 µm size, and then the sphene particles were sprayed onto Ti-6Al-4V discs (10×10×2 mm; Xi'an Continental Biomaterials Ltd Cor, China), using an atmosphere plasma spray system (APS-2000, Switzerland) and the parameters shown in table 1. Plasma-sprayed HAp coatings on Ti-6Al-4V substrates (HAp particle size: 45–160 µm) were prepared with same preparation conditions and used with uncoated Ti-6Al-4V as the controls. For cell culture, the Ti-6Al-4V discs were ultrasonically washed with water, acetone and ethanol for 10 min, respectively, and then dried at 40°C overnight.

2.2. Characterization of coating

The phase composition of the Ti-6Al-4V substrates before and after coating was analysed using X-ray diffraction (XRD; Siemens D5000, Germany) with a step size of 0.02° at a scanning rate of 1.2° min⁻¹. Surface morphology and roughness of the Ti-6Al-4V-coated discs were analysed using scanning electron

microscopy (SEM; Philips XL 30 CP, The Netherlands) and atomic force microscopy (AFM; Tempe, AZ, USA) in tapping mode. For evaluation of the coating thickness, inner microstructure and bonding interface, the coated discs were fixed in polymethylmethacrylate (PMMA) and sections were cut using a diamond saw (Exakt 300CL, Exakt Apparatebau, Germany) and subsequently ground and polished with an Exakt 400 CS Micro Grinding System (Exakt Apparatebau, Germany) before analysing by SEM. The open porosity of the coatings was tested by Archimedes' method.

2.3. Bonding strength and chemical stability of coating

For measuring the bonding strength, sphene coating with a thickness of approximately 380 µm was sprayed on Ti-6Al-4V rods with a diameter of 25 mm. The bonding strength between the coating and Ti-6Al-4V was measured in accordance with American Society for Testing and Materials C-633 (Liu *et al.* 2002; Xue *et al.* 2004).

For evaluation of the chemical stability of the coating, the coated discs were soaked in a buffer solution of tris(hydroxymethyl)aminomethane (Tris, (CH₂OH)₃CNH₂) and hydrochloric acid (HCl), with pH 7.4, for 1, 3 and 7 days, and the ratio of disc surface area and solution volume of Tris-HCl was 0.1 cm² ml⁻¹. After soaking, the change of ion concentrations in Tris-HCl solution was analysed using inductively coupled plasma atomic emission spectroscopy (ICP-AES; Optima 3000 DV, PerkinElmer, USA) and the dissolution kinetic constant was calculated according to the released ion concentrations. The morphology of coating after soaking was analysed by SEM.

2.4. Isolation and culture of human osteoblast-like cells

HOB were grown from small pieces of vertebral bone harvested from healthy patients under 15 years of age undergoing orthopaedic procedures (Wu *et al.* 2007a,b, 2008a–c, 2008). Bone was morselized into approximately 1 mm³ pieces, washed several times with phosphate-buffered saline (PBS) and digested for 90 min at 37°C with 0.02 per cent (w/v) trypsin (Sigma) in PBS. The digested cells were cultured in α -minimal essential medium (α -MEM; Gibco Laboratories), supplemented with 10 per cent (v/v) foetal calf serum (FCS; Gibco Laboratories), 2 mM L-glutamine (Gibco Laboratories, Grand Island, NY, USA), 25 mM Hepes buffer (Gibco Laboratories), 2 mM sodium pyruvate, 30 mg ml⁻¹ penicillin, 100 mg ml⁻¹ streptomycin (Gibco Laboratories) and 0.1 M L-ascorbic acid phosphate magnesium salt (Wako Pure Chemicals, Osaka, Japan). Then the digested cells were cultured in 75 cm² flasks at 37°C in a CO₂ incubator until confluence (approx. 70 per cent). The confluent cells were trypsinized and used for the attachment, proliferation and alkaline phosphatase assays. Permission to use discarded human tissue was granted by the Human Ethics Committee of the University of Sydney.

2.5. Attachment and morphology of HOB

HOB was cultured on sphene and HAp-coated Ti-6Al-4V discs placed in a 24-well culture plate at an initial density of 1×10^4 cells cm⁻². Cells were then incubated for 1, 3 and 7 days in α -MEM culture medium supplemented with 10 per cent FCS in humidified culture conditions. At the completion of culture, the discs were removed from the culture wells, rinsed with PBS (pH 7.4) and fixed with 1.25 per cent glutaraldehyde, 4 per cent paraformaldehyde and 4 per cent sucrose in PBS for 1 hour. The fixative was removed by washing with a buffer containing 4 per cent (w/v) sucrose in PBS and post-fixed in 1 per cent osmium tetroxide in PBS followed by sequential dehydration in graded ethanol (30, 50, 70, 90, 95, 100 per cent). Specimens were dried in hexamethyldisilizane for 3 min before coating with gold for SEM analysis. The morphological characteristics of attached cells on the coating discs were determined using SEM.

After 7 days of culture, the medium was collected from each well and ion concentrations were measured using ICP-AES.

2.6. Proliferation of HOB

The mitochondrial activity of the HOB cultured on coating and Ti-6Al-4V discs was determined by colorimetric assay, which detected the conversion of 3-(4,5-dimethylthiazol-2-yl)-2,5-diphenyltetrazolium bromide (MTS; Promega, Madison, WI, USA) to formazan, as detailed previously (Wu *et al.* 2008a–c, 2008). Cells were harvested with 0.1 per cent trypsin-EDTA solution in PBS and resuspended in full culture medium as detailed above. The cells were seeded at a concentration of 5×10^4 cells cm⁻² onto the coating and the Ti-6Al-4V discs placed individually in a 24-well plate. Then the cells were left to grow for 1, 3 and 7 days at 37°C in a humidified atmosphere of 95 per cent air and 5 per cent CO₂. HAp-coated Ti-6Al-4V discs, uncoated Ti-6Al-4V discs and tissue culture plastic (TCP) templates were used as control. At days 1, 3 and 7, the discs were previously washed with 1× PBS. Freshly prepared MTS reaction mixture was diluted in PBS at a volume ratio of 1 : 5 (MTS : PBS) and added to the wells containing the discs and incubated at 37°C for 4 hours. Three specimens of each type were tested for each culture time point. One hundred microlitres of the converted 3-(4,5-dimethylthiazol-2-yl)-2,5-diphenyltetrazolium bromide from each well were transferred to a 96-well plate and the absorbance was recorded using a microplate reader (PathTech) at 490 nm using the software ACCENT.

2.7. Alkaline phosphatase (ALP) activity of HOB

The functionality of HOB cultured on the test and control discs was assessed by measuring the ALP activity using *p*-nitrophenyl phosphate substrate (ALP kit; Thermochem). The HOB were plated at a density of 5×10^4 cells cm⁻² on the various discs and cultured for 1, 3 and 7 days. At the predetermined time point, the culture medium was decanted and the cell layer washed gently three times with 1× PBS followed by washing once with cold 50 mM Tris buffer, before lysing in Tris buffer containing 0.2 per cent NP-40

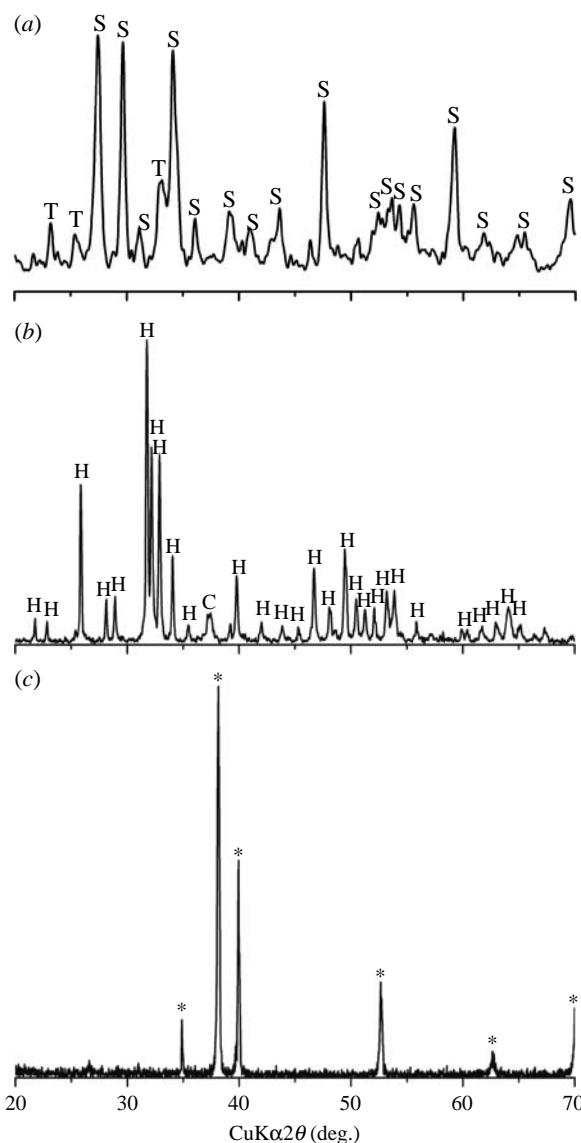


Figure 1. XRD analysis of (a) sphene and (b) hydroxyapatite coating and (c) Ti-6Al-4V substrates (asterisk denotes Ti-6Al-4V). S, sphene; T, CaTiO₃; H, HAp; C, CaO.

solution. The cells were sonicated for 20 s, centrifuged at 3000*g* for 5 min at 4°C and 2 µl of the lysate were added to 100 µl of 16.3 mmol l⁻¹ *p*-nitrophenyl phosphate (Thermochem) in a 96-well plate and incubated for 30 min at 37°C. Reactions were stopped using 100 µl of 0.1 N NaOH and the absorbance read at 405 nm using a microplate reader (PathTech). The ALP activity was calculated from a standard curve after normalizing to the total protein content, which was measured using Pierce BCA protein assay kit, and the results expressed in millimolar *p*-nitrophenyl phosphate produced per minute per milligram of protein. ALP experiments were performed in triplicate and triplicate discs were used in each experiment.

2.8. Statistical analysis

The data were expressed as means \pm standard deviation (s.d.) for all experiments and analysed using one-way ANOVA with *post hoc* test; *p* < 0.05 was considered statistically significant.

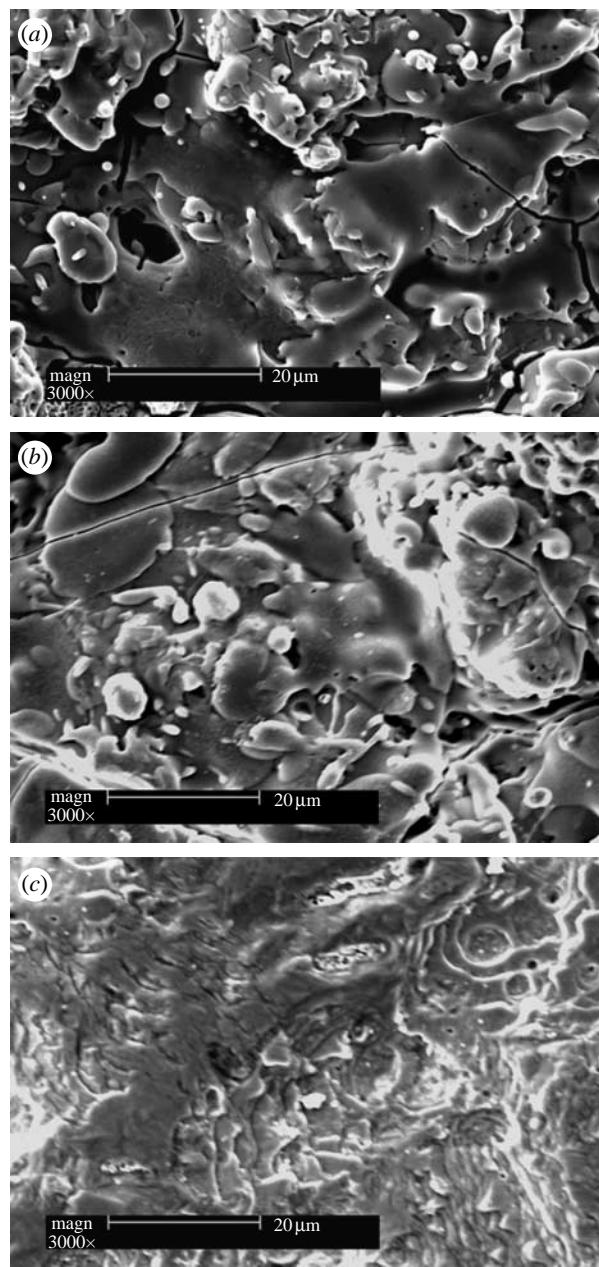


Figure 2. SEM morphology of (a) sphene and (b) hydroxyapatite coating and (c) Ti-6Al-4V discs.

3. RESULTS

3.1. Characterization of coating

XRD analysis shows that before coating, there are only characteristic peaks of Ti in the pattern (figure 1c), and after coating, sphene characteristic peaks (standard card no. JCPD 11-0142) and weak peaks of CaTiO₃ exist in the pattern of plasma-sprayed sphene coating (figure 1a). The plasma-sprayed HAp coating contains mainly HAp crystal phase (standard card no. JCPD 24-0033) and CaO phase in only minor amounts (figure 1b).

After plasma spray coating, the surface morphology of the Ti-6Al-4V discs changed significantly (figure 2). A compact sphene coating composed of melted sphene particles formed on the Ti-6Al-4V discs (figure 2a), with a morphology similar to that of the HAp coating (figure 2b). AFM analysis demonstrated that sphene-coated Ti-6Al-4V possesses a surface roughness similar

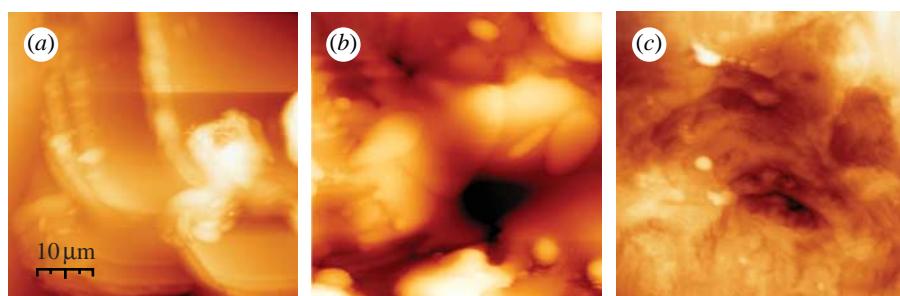


Figure 3. AFM analysis of the surface roughness: (a) sphene coating ($R_a=10\text{ }\mu\text{m}$), (b) HAp coating ($R_a=10\text{ }\mu\text{m}$) and (c) Ti-6Al-4V substrates ($R_a=0.5\text{ }\mu\text{m}$).

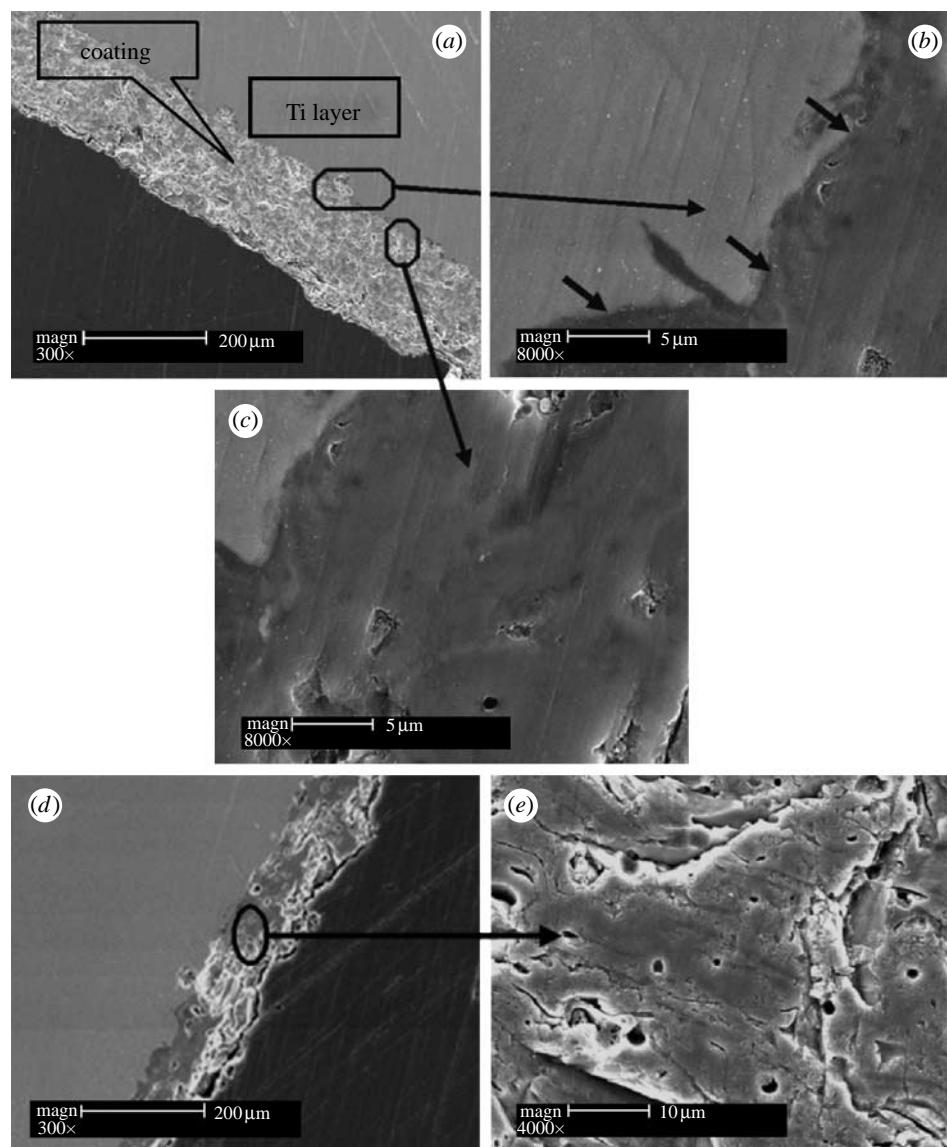


Figure 4. SEM cross section of sphene and HAp coating. (a) Thickness of sphene coatings is approximately 150 μm , (b) sphene coating and Ti-6Al-4V substrates forming a close interface as shown by arrows and (c) sphene coating possessing dense structure. (d) Cross section and (e) inner structure of HAp coatings.

to that of the HAp coating (10 μm), and both were significantly higher than that for the uncoated Ti-6Al-4V discs (0.50 μm ; figure 3). The corresponding polished cross sections of the sphene and HAp coating are shown in figure 4. The thickness of the coating is approximately 150 μm (figure 4a). No microcracks were observed at the interface, indicating a close bonding between the coating

and the Ti-6Al-4V substrates (figure 4b). The inner microstructure of sphene coating is highly dense and only a few micropores existed (figure 4c). The thickness of the HAp coating is approximately 140 μm (figure 4d) and a few micropores existed in the inner structure (figure 4e). The open porosity of the sphene and HAp coatings is 1.77 ± 0.34 per cent and 3.04 ± 0.66 per cent, respectively.

Table 2. Bonding strength of plasma-sprayed sphene and HAp coating.

coating	bonding strength (MPa)	references
plasma-sprayed sphene	33.2 ± 2.4	
sol-gel sphene	17.4 ± 0.9	Wu <i>et al.</i> (2008a-c, 2008)
plasma-sprayed HAp	5.9	Tsui <i>et al.</i> (1998)
	8.0–16.6	Khor <i>et al.</i> (1997, 1998)
	13.0	Zheng <i>et al.</i> (2000)
	24.5	Kweh <i>et al.</i> (2002)

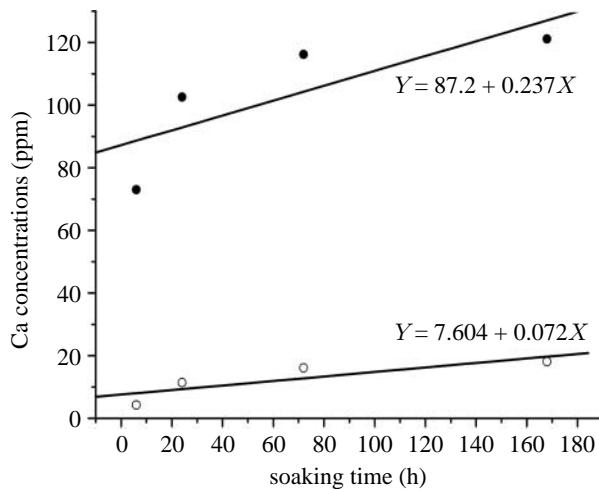


Figure 5. Ca dissolution kinetics of sphene (open circles) and HAp (filled circles) coating after 1, 3 and 7 days soaking in Tris-HCl solution by ICP-AES analysis.

3.2. Bonding strength and chemical stability of coating

The bonding strength of the plasma-sprayed sphene coating on Ti-6Al-4V was 33.2 ± 2.4 MPa (table 2). ICP-AES analysis of Ca dissolution kinetics of the plasma-sprayed sphene and HAp coatings in Tris-HCl solutions is shown in figure 5. The concentration of the released Ca ions in Tris-HCl solution for sphene coating is significantly lower than that for HAp coating. Sphene coating has a lower dissolution kinetics constant ($k=0.072 \text{ ppm h}^{-1}$) compared with that of HAp coating ($k=0.237 \text{ ppm h}^{-1}$). SEM morphology analysis shows that after soaking in Tris-HCl for 7 days, sphene coating has no obvious change (figure 6a). However, the surface of HAp coating becomes coarse with some evidence of microparticles (figure 6b).

3.3. Attachment and morphology of HOB on coating

HOB attachment and morphology on sphene and HAp coating were examined using SEM. Sphene and HAp coatings supported HOB attachment after 1 and 3 days of culture (figure 7a-d) and cells were confluent and well spread on the two coatings after 7 days of culture (figure 7e-h).

3.4. Proliferation and ALP activity of HOB

At day 3, HOB proliferation on sphene coating is a little lower than that on HAp coating and comparable

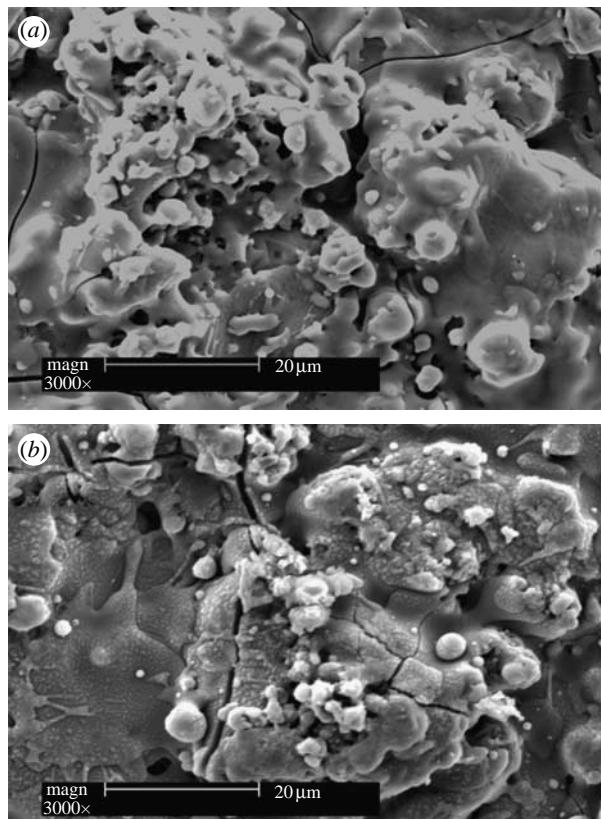


Figure 6. SEM morphology of (a) sphene and (b) hydroxyapatite coating after soaking in Tris-HCl for 7 days.

to Ti-6Al-4V and TCP (figure 8). However, by day 7, the HOB cultured on sphene-coated Ti-6Al-4V exhibited a significantly higher ($p<0.05$) proliferation than that on HAp coating, Ti-6Al-4V and TCP (figure 8). Figure 9 illustrates the changes in ALP activity of the HOB cultures at 1, 3 and 7 days. On days 1 and 3, the ALP activity is expressed at low levels for both sphene coating and controls. Thereafter, the ALP activity increased over time, and by day 7 was significantly higher ($p<0.05$) on sphene coating compared with HAp coating, Ti-6Al-4V and tissue culture plate (figure 9).

3.5. Ion concentration of culture medium

After 7 days of culture, the concentrations of Ca and Si ions in sphene coating-cultured medium are 2.85 and 0.29 mM, respectively, and no Ti ions are detected. There are no Si ions in HAp coating-cultured medium and TCP (table 3).

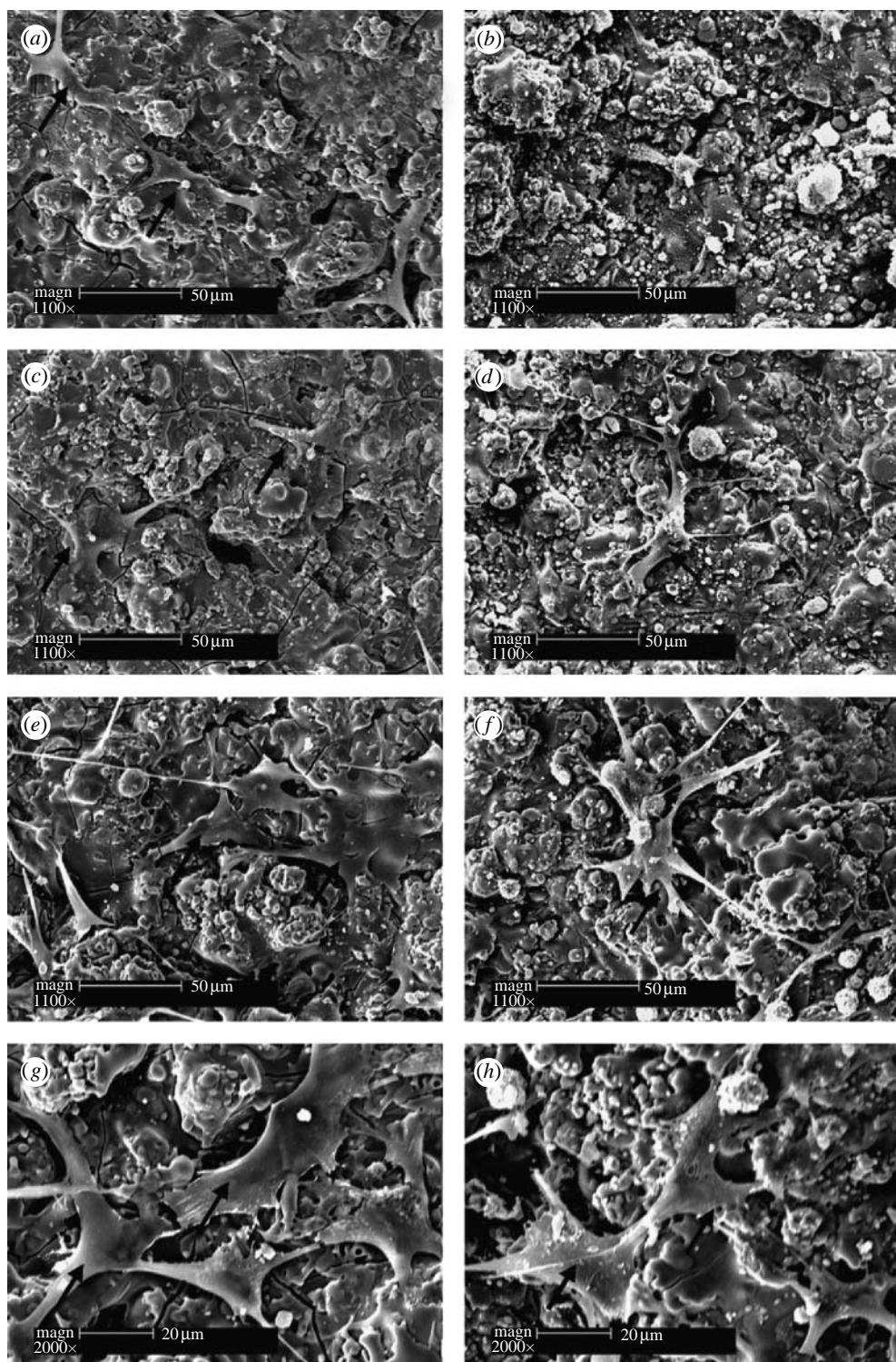


Figure 7. SEM of the attachment and morphology of human bone-derived cells cultured on sphene coating for (a) 1, (c) 3 and (e,g) 7 days, and on HAp coating for (b) 1, (d) 3 and (f,h) 7 days. (g) and (h) are higher magnification images. Arrows indicate cells.

4. DISCUSSION

The major finding of this study is that we developed for the first time the plasma-sprayed sphene-coated Ti-6Al-4V with significantly improved bonding strength, chemical stability and cellular bioactivity compared with the currently used HAp coating. HAp- and CaSiO₃-coated orthopaedic and dental implants have been widely studied for clinical trials and applications (Bauer *et al.* 1991; Kweh *et al.* 2002; Xue *et al.* 2005;

Fini *et al.* 2008). However, the main drawbacks of these coatings are their poor bonding strength and insufficient chemical stability, which result in the delamination of coating from Ti alloys and limits their long-term survival (Khor *et al.* 1997; Kweh *et al.* 2002; Liu *et al.* 2004a,b; Xue *et al.* 2004). An important characteristic feature of a coated implant material is its sufficient bonding strength and chemical stability to maintain long-term functional loading. We showed that Ti-6Al-4V plasma-coated with

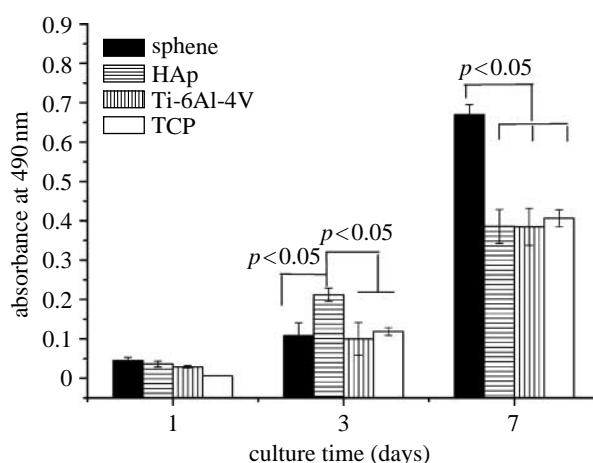


Figure 8. HOB proliferation on sphene, HAp coating and Ti-6Al-4V substrates at 1, 3 and 7 days of culture. TCP, tissue culture plate.

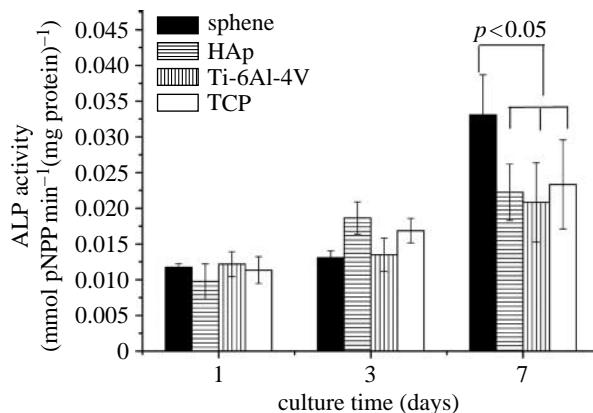


Figure 9. ALP activity of HOB on sphene, HAp coating and Ti-6Al-4V substrates at 1, 3 and 7 days of culture. TCP, tissue culture plate.

sphene possessed a significantly higher bonding strength (33.2 MPa), compared with HAp-coated Ti-6Al-4V (5.9–24.5 MPa; Khor *et al.* 1997, 1998; Tsui *et al.* 1998; Zheng *et al.* 2000; Kweh *et al.* 2002) and the sol-gel sphene coating (17.4 MPa; Wu *et al.* 2008a–c, 2008).

There are two important reasons for the excellent bonding strength of sphene plasma coating. One is the dense microstructure of sphene plasma coating. Previous studies have shown that the porosity of a coating has a significant effect on the bonding strength (Liu *et al.* 2004a,b; Oh *et al.* 2005). In this study, the porosity of sphene plasma coating (1.77 per cent) is lower than that of HAp plasma coating (3.04 per cent), which may contribute to the improved bonding strength of sphene plasma coating compared with HAp plasma coating. The sintering properties and powder shape may be the main factors affecting the coating density. Different ceramics have different sintering properties, such as sintering kinetics and shrinkage, at high temperature. Sphene may have better sintering properties that result in higher density. Although sphene and HAp powders have similar size distribution, however, the shape of powders may be a little different. Powder shape will affect powder flowability and further affect the coating density (Bartuli *et al.* 2002). In addition, the plasma spraying technique

Table 3. Ion concentrations of culture medium after 7 days of culturing HOB on coating and tissue culture plate (TCP).

coating	ion	concentration (mM)
sphene	Ca	2.85
	Si	0.29
	Ti	0
HAp	Ca	4.95
	Si	0
TCP	Ca	2.40
	Si	0

produced sphene coating with denser microstructure than the sol-gel technique. We recently demonstrated that sol-gel sphene coating possesses excellent chemical stability and enhanced bonding strength compared with sol-gel HAp-coated Ti-6Al-4V (Wu *et al.* 2008a–c, 2008). However, the sol-gel sphene coatings can only be sintered at relatively low temperature (less than 900°C) as higher temperature (more than 900°C) sintering will oxidize and damage the surface of the metal. The problem with low temperature (less than 900°C) sintering is that we cannot produce a completely dense structure of the sol-gel sphene coating, thus affecting its bonding strength. Plasma spraying is by far the most frequently used commercial technique for coating biomedical devices. The advantages of plasma spraying, compared with the sol-gel technique, include high deposition rates (80 g min⁻¹) and rough surface, which is favourable for bone substitutes (Liu *et al.* 2004a,b). The plasma spraying technique uses higher temperature compared with sol-gel coatings, producing dense microstructure and thereby denser bonding interface (Liu *et al.* 2004a,b).

Thermal expansion coefficient of ceramics (Saiz *et al.* 2002; Liu *et al.* 2004a,b) is another parameter that influences the bonding strength between the coatings and the underlying substrata. Sphene ceramics (6×10^{-6} K⁻¹) possess a thermal expansion coefficient similar to that of Ti-6Al-4V (8.4×10^{-6} to 8.8×10^{-6} K⁻¹), therefore favouring a higher bonding strength and reducing the residual stress, which may result from the mismatch of the thermal expansion coefficient.

The chemical stability of the ceramics is an important factor influencing the long-term stability of the coating (Liu *et al.* 2004a,b; Wu *et al.* 2007a,b). In this study, we found that plasma-sprayed sphene coating has a decreased dissolution rate compared with HAp coating, indicating that sphene coating possesses an improved chemical stability, compared with HAp coating. Previous studies showed that the crystal structure of the ceramics affect their stability (Ducheyne *et al.* 1993; Radin & Ducheyne 1994). It is known that sphene and HAp ceramics have different crystal structures (sphene, monoclinic; HAp, hexagonal), which may result in the difference of the chemical stability of the two ceramic coatings.

The interaction of the cells with their substrate is a key factor for cellular activity including attachment, proliferation and differentiation (Anselme 2000), ultimately determining the cellular phenotype on the

biomaterials. The results of the present study indicate that plasma-sprayed sphene-coated Ti-6Al-4V supported HOB attachment and spreading, and significantly enhanced HOB proliferation and ALP activity compared with plasma-sprayed HA₁ coating and uncoated Ti-6Al-4V substrates, indicating an excellent cellular bioactivity. Zreiqat *et al.* have shown that chemical composition (Zreiqat *et al.* 2002, 2005; Wei *et al.* 2008) and surface topography (Liu *et al.* 2008) of the biomaterial can alter the cellular responses substantially. The chemical composition of the plasma-sprayed sphene coating is significantly different from that of the HA₁ coating and the Ti-6Al-4V substrates. Moreover, we found that sphene and HA₁-coated Ti-6Al-4V have similar surface topography and roughness, but differ significantly in their chemical composition. Sphene is a Ca-, Ti- and Si-containing ceramic, while HA₁ is a Ca- and P-containing ceramic. Therefore, it is plausible to speculate that the different chemical composition between the two ceramics (sphene versus HA₁) is the major contributor to the differences seen in the cellular responses to both coatings.

Previous studies have shown that ionic environment, caused by the dissolution of ions from biomaterials, has an important impact on the biological responses of cells (Valerio *et al.* 2004; Wu *et al.* 2005). Differences in materials' chemical composition will result in different ionic environments (Wu *et al.* 2006, 2007a,b) presented to the cells. Ions such as Ca and Si play a significant role in stimulating osteoblast proliferation, differentiation and regulation of their gene expression (Silver *et al.* 2001; Wu & Chang 2007; Wu *et al.* 2007a,b). In the present study, minor amounts of Ca and Si ions were released from the sphene coating (table 3), which may have contributed to the improved cellular activity. In addition, we found no detectable levels of Ti ions in the culture medium (Ti ion concentration was lower than the testing limit of ICP-AES (0.00X ppm)). Normal concentration of Ti in human tissue is 0.2 ppm (Hildebrand & Hornez 1998), and around the titanium implants no clinical tissue toxicity has been observed at local Ti concentrations of higher than 2000 ppm (Hildebrand & Hornez 1998). Therefore, the trace amount of Ti ions released from the sphene coating is very unlikely to result in toxic effects on human tissue.

5. CONCLUSIONS

Plasma-sprayed sphene coating on Ti-6Al-4V has been successfully prepared and demonstrates a close bonding with the Ti-6Al-4V substrate. The coating possesses a significantly improved bonding strength and chemical stability and enhanced HOB proliferation and differentiation, compared with plasma-sprayed HA₁ coating and uncoated Ti-6Al-4V. Taken together, plasma-sprayed sphene coating on Ti-6Al-4V possessed excellent bonding strength, chemical stability and cellular bioactivity, indicating its potential application as a coating for orthopaedic implants.

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